

Dynamic Cell and Microparticle Control via Optoelectronic Tweezers

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Abstract—This paper reports on cell and microparticle manipulation using optically induced dielectrophoresis. Our novel optoelectronic tweezers (OET) device enables optically controlled trapping, transportation, and sorting via dielectrophoretic forces. By integrating a spatial light modulator and using direct imaging, arbitrary dynamic manipulation patterns are obtained. Here, we demonstrate manipulation functions, including particle collectors, single-particle traps, individually addressable single-particle arrays, light-defined particle channels, and size-based particle sorting. OET-induced particle manipulation velocities are analyzed as a function of the applied voltage, optical pattern linewidth, and single-particle trap dimensions. [2006-0210]

Index Terms—Dielectrophoresis (DEP), optical tweezers, optically induced DEP, optoelectronic tweezers (OET).

I. INTRODUCTION

MICROSCALE manipulation is an important tool in many fields, including biological research and colloidal science. Dynamic easily reconfigurable micromanipulation tools are highly sought.

One mature cellular-scale manipulation technology is optical tweezers, which provides a noninvasive method of manipulating particles with sizes from approximately 100 μm down to a few nanometers [1]. Holographic techniques have been used to increase the functionality of optical tweezers to include particle sorting [2], 3-D manipulation [3], and the creation of multiple optical traps [4], [5]. However, optical tweezers are limited by high optical power requirements. A typical trap requires at least 1 mW of laser power, whereas the multiple traps created by holographic optical tweezers demand source powers of 500 mW to 1 W [5], [6]. Such high power levels, especially in the visible wavelengths, can result in optical and/or thermal damage to live biological specimens [7]–[12]. Furthermore, as optical tweezers relies on the gradient force of the optical beam to trap particles, the laser light must be highly focused. Typically, high-numerical-aperture lenses are employed to achieve optical trapping, limiting the manipulation area of most optical tweezers to a field of view of less than 100 μm . This represents

a bottleneck in the parallel processing of biological cells (which may have diameters of 10 μm or greater) and larger particles. Optical tweezers are also limited to attractive forces for most biological particles such as cells.

Dielectrophoresis (DEP) is another widely used microparticle manipulation technique [13]. It has been demonstrated on particles with sizes ranging from approximately 1 mm down to 14 nm [14]. Unlike optical tweezers, DEP is capable of a large effective particle manipulation area, is limited only by the size of the device, and can produce repulsive forces in addition to attractive forces. However, a limitation of conventional DEP is the static pattern of electrodes used for particle manipulation, reducing the flexibility of this technology.

We have demonstrated another method for the optical manipulation of micrometer-scale objects: optically induced DEP or optoelectronic tweezers (OET) [15]. Using a laser to induce dielectrophoretic forces, we have demonstrated controlled movement of 25- μm polystyrene particles and *E. coli* bacteria [16], [17]. This technique allows the use of very low optical power levels, enabling particle manipulation with an incoherent light source. The integration of a spatial light modulator into the optical system enables dynamic reconfigurable optical patterns, providing increased functionality and versatility in particle manipulation. Using incoherent-light-actuated OET, we have demonstrated the creation of 15 000 particle traps over an area of 1.3 mm², size-based particle sorting, and the selective concentration of live and dead human B cells [15]. In addition, another group has used optically induced DEP to form virtual channels and to trap yeast cells [18]–[20].

In this paper, we present the dynamic direct-image-driven manipulation of live red and white blood cells and microparticles using incoherent-light-driven OET. We demonstrate many particle manipulation techniques, including particle collectors, single-particle traps, individually addressable single-particle arrays, light-defined particle channels, and size-based particle sorting. Critical parameters for the optimization of OET manipulation patterns are analyzed, including the dependence of the OET-induced manipulation velocity on applied voltage, optical pattern linewidth, and single-particle trap dimensions.

II. DEP

The actuation forces of OET are identical to those of DEP, which refers to the forces induced upon a particle in the presence of a nonuniform electric field [13]. A particle within the electric field forms an induced dipole, which experiences

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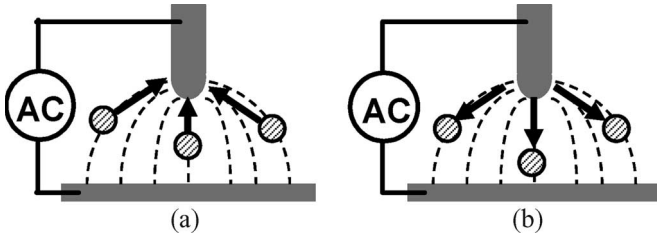


Fig. 1. Frequency dependence of dielectrophoretic force. (a) Positive DEP, in which particles are attracted toward electric field maxima, occurs when $\text{Re}[K(\omega)] > 0$. (b) Negative DEP, in which particles are repelled from field maxima, occurs when $\text{Re}[K(\omega)] < 0$.

a force dependent upon the field gradient (for a spherical particle), i.e.,

$$F_{\text{DEP}} = 2\pi r^3 \epsilon_m \text{Re}[K(\omega)] \nabla(E^2) \quad (1)$$

where r is the particle radius, ϵ_m is the permittivity of the media surrounding the particle, E is the root-mean-square value of the electric field, and $\text{Re}[K(\omega)]$ is the real part of the Clausius–Mossotti factor, i.e.,

$$K(\omega) = \frac{\epsilon_p^* - \epsilon_m^*}{\epsilon_p^* + 2\epsilon_m^*}, \quad \epsilon_p^* = \epsilon_p - j\frac{\sigma_p}{\omega}; \quad \epsilon_m^* = \epsilon_m - j\frac{\sigma_m}{\omega} \quad (2)$$

where σ is the conductivity of the particle or the medium, and ω is the angular frequency of the electric field. The magnitude of $\text{Re}[K(\omega)]$ varies with frequency, resulting in frequency dependence of the dielectrophoretic force (Fig. 1). Positive values of $\text{Re}[K(\omega)]$ result in particle attraction to electric field maxima (positive DEP). For negative values of $\text{Re}[K(\omega)]$, particles are repelled from field maxima (negative DEP). Applying an ac electric field thus allows the tuning of the type of DEP force induced on a particle, as well as negating any electrophoretic effects, or particle movement due to its surface charge.

In conventional DEP, the nonuniform electric fields are generated by a variety of static electrode configurations [21]–[23]. To create dynamic nonuniform fields for reconfigurable DEP traps, complex control circuitry using CMOS technology is required [24]. In contrast, optoelectronics tweezers enable light-patterned virtual electrodes to address dielectrophoretic forces. It is flexible and reconfigurable and can continuously address DEP forces across a 2-D surface.

III. OET

A. Device Structure and Fabrication

The lower photoconductive surface of the OET device consists of an indium–tin–oxide (ITO)-coated glass substrate, a 10-nm aluminum film to reduce contact resistance, a 1- μm undoped amorphous silicon (a-Si) photoconductive layer, and a 20-nm silicon nitride passivation layer. A liquid solution containing the particles of interest is sandwiched between the photoconductive surface and an upper ITO-coated glass slide (Fig. 2). A 100- μm spacer is used to maintain the gap between the upper and lower surfaces. An ac bias across the top and bottom ITO layers is applied to power the device.

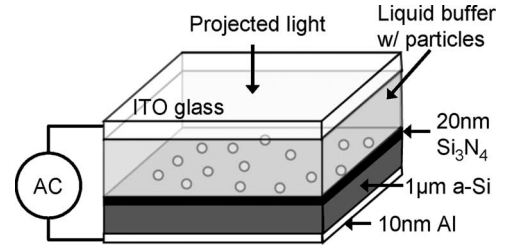


Fig. 2. OET device structure. A liquid solution containing the particles of interest is contained between an upper electrode surface (ITO glass) and a lower photoconductive layer (a-Si), separated by a 100- μm spacer (not shown).

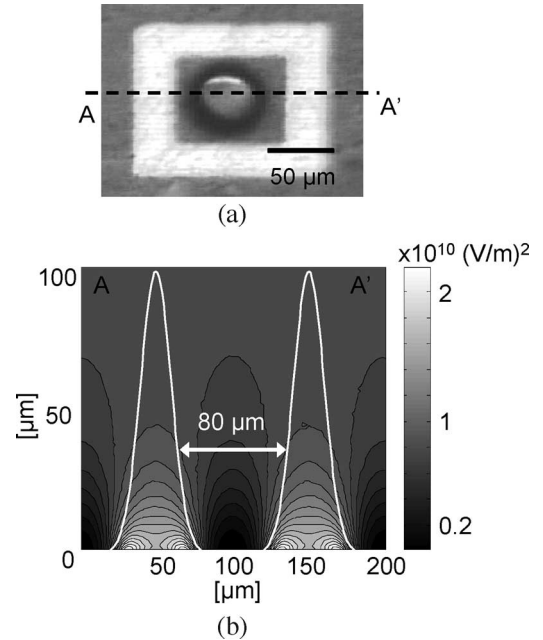


Fig. 3. (a) Single-particle OET trap. A 45- μm polystyrene sphere is contained by optically induced negative DEP. (b) Distribution of the square of the electric field for the single-particle trap along the cross section A–A'. The DEP force is proportional to the gradient of this distribution. The profile of the projected 20- μm -wide light pattern, which is approximated by Gaussian beams, is represented by the white lines.

B. Optically Induced DEP

The OET device enables optically induced DEP by exploiting the photoconductive properties of the amorphous silicon layer. Amorphous silicon has a very high electrical impedance in the dark; thus, most of the applied voltage drops across the a-Si layer, resulting in a low electric field in the liquid layer. However, focusing incident light onto the a-Si surface creates electron–hole pairs, reducing the impedance of a-Si layer by several orders of magnitude. As a result, a “virtual electrode” is created in the illuminated area. This switches the majority of the voltage drop to the liquid layer, forming a high electric field in the liquid above the virtual electrode. The resulting electric field gradient in the liquid layer creates dielectrophoretic force for microparticle manipulation.

To illustrate, a repulsive OET trap is shown in Fig. 3(a). This single-particle rectangular trap has inner dimensions of $80 \times 60 \mu\text{m}$. A sphere with a diameter of $45 \mu\text{m}$ is surrounded by light “walls” $20 \mu\text{m}$ in width. The corresponding cross-sectional distribution of the square of the electric field was

TABLE I
MULTIPHYSICS SIMULATION PARAMETERS

Parameter	Value
a-Si peak conductivity	100 mS/m
a-Si relative permittivity	11
Liquid conductivity	10 mS/m
Liquid relative permittivity	80
Applied voltage	10 V
FWHM beam width	20 μm

simulated using a commercial finite-element modeling program (FEMLAB, now COMSOL Multiphysics [25]). The simulation parameters are based on empirically determined material properties and are given in Table I. The conductivity of the a-Si is assumed to be proportional to the illuminated light intensity, with a peak value of 100 mS/m. The intensity of the illumination patterns is assumed to have a Gaussian profile. The simulation result shows that the width of the trap as experienced by the particle is approximately 50 μm , as DEP force depends on the gradient of this distribution [Fig. 3(b)]. If negative DEP forces are induced by the trap pattern, all particles outside the trap area will be repelled by the electric field maxima forming the trap perimeter. Any particle within the enclosed trap area will feel similar repulsive forces, but these forces balance, trapping the particle. Once a particle is contained within the rectangular pattern, the trap can be moved, transporting the particle to a desired location. Furthermore, multiple traps can be used as building blocks to form arrays of trapped particles. Such arrays can be arbitrarily arranged and dynamically reconfigured.

C. Experimental Setup

Polystyrene beads of various sizes (5-, 10-, 20-, 25-, or 45- μm diameters, from Polysciences, Inc.) are suspended in a liquid solution consisting of deionized water and KCl salt, which are mixed to obtain a conductivity of 10 mS/m. Live bovine red blood cells or live human B cells are suspended in an isotonic solution of 8.5% sucrose and 0.3% dextrose. The suspended cells or microparticles are introduced into the OET device, which is placed on a microscope for observation. A charge-coupled device (CCD) camera that is attached to the observation port of the microscope records images and video of the experiments. To produce the electric field that is necessary for DEP, an ac voltage (Agilent 33120A) is applied across the top ITO surface and the bottom photoconductive surface of the OET device.

The light source in some prior OET experiments consisted of a 0.8-mW He-Ne laser [16], [17]. However, the low optical power requirement of OET enables the use of an inexpensive incoherent light source such as a mercury or halogen lamp or a LED (Fig. 4).

In addition, we can produce light patterns by imaging technique rather than scanning technique. With no need to focus all optical energy, we can use a spatial light modulator to directly pattern images rather than the holographic techniques that are employed by optical tweezers arrays [4]–[6]. Our current setup uses a 1024 \times 768 pixel digital micromirror device (DMD)

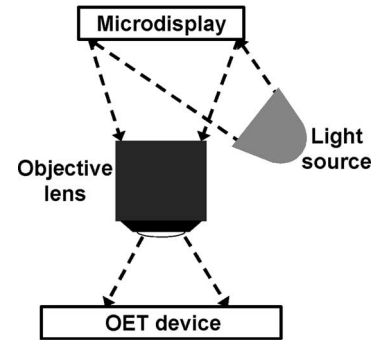


Fig. 4. Experimental setup for OET. The light source is incoherent (mercury or halogen lamp or LED).

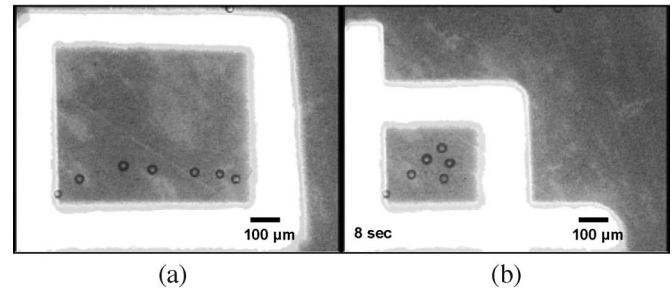


Fig. 5. Collection of 25- μm -diameter polystyrene beads in a solution via negative DEP. The incoherent light patterns are generated with a micromirror array and projected onto the OET device.

from Texas Instruments. Each pixel of the DMD is 13.68 \times 13.68 μm . The image from the DMD is focused using a 10 \times objective lens (NA = 0.30) and projected onto the OET device. Control of the projected images is accomplished via a PC interface to the DMD.

IV. EXPERIMENTAL RESULTS

A. Microparticle Manipulation

One type of optical setup for OET manipulation using an incoherent light source is a DMD-based digital projector (InFocus LP335). The projector displays images that are drawn on a PC in Microsoft PowerPoint software. In this setup, the projector provides both the optical source (a high-pressure mercury lamp) and the DMD-to-PC interface. The output of the projector is collected, collimated, and directed into the 10 \times objective lens, projecting an image onto the OET device. The power at the projector output was measured to be approximately 600 mW. Approximately 7% of this power is collected by the objective lens and focused onto the OET surface. Therefore, the power of the light incident on the OET surface (not including losses through the bulk optics) is 42 mW, corresponding to an intensity of 120 nW/ μm^2 .

Negative DEP forces were employed to collect randomly distributed particles (Fig. 5). As the light pattern sweeps across the manipulation area, particles are pushed into the desired location.

Using different image patterns, we were able to create dynamic single-particle ring traps containing a single 25- μm

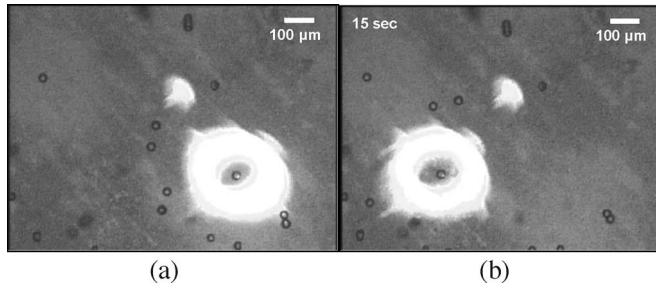


Fig. 6. (a) Single-particle trap is formed using negative DEP. (b) As the light pattern is moved, a single 25- μm -diameter polystyrene bead remains in the trap, whereas the beads outside the trap are repelled.

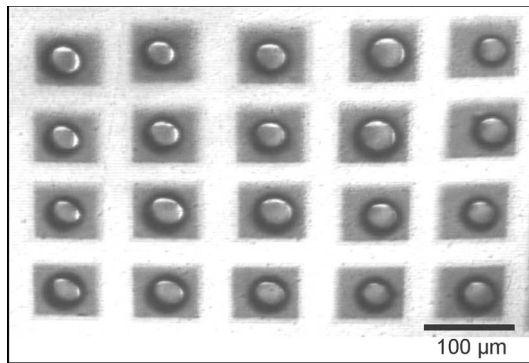


Fig. 7. Array of single 45- μm -diameter beads formed from multiple single-particle square traps. Each particle is individually addressable. The time required to form this array of 20 particles was 3 min.

diameter polystyrene bead via negative DEP (Fig. 6). These traps were translated in real time under user control, at velocities of up to 40 $\mu\text{m}/\text{s}$.

Using multiple instances of these single-particle traps, individually addressable arrays of particles can be formed. Each randomly positioned particle is first contained within a square trap, which is a procedure achieved in real time by manual user control of the image pattern. The multiple traps can then be positioned to form an array of individually addressable cells. Using this technique, we were able to form a 5×4 array of single-particle traps (Fig. 7). We were able to move the resulting array of single particles around the image plane at approximately 25 $\mu\text{m}/\text{s}$. Although the formation of the array was performed manually, it can be automated by combining OET with an image-analysis feedback-control system, as demonstrated in [26] and [27]. Biological applications of such an array include studies on single-cell behavior and interactions.

Since each cell of the array is an independent single-particle trap, the array has the capability of being dynamically rearranged. To illustrate, an array consisting of 45- and 20- μm polystyrene beads is reorganized under operator control (Fig. 8). This demonstrates the addressability of each particle trap, as well as the dynamic nature of the OET patterns.

By adjusting the projected image, other particle manipulation schemes are achievable. Negative DEP can be used to guide particles along light-defined “channels” at velocities of approximately 10 $\mu\text{m}/\text{s}$ (Fig. 9). In addition, due to the ease of reconfiguration of the manipulation pattern, we can implement

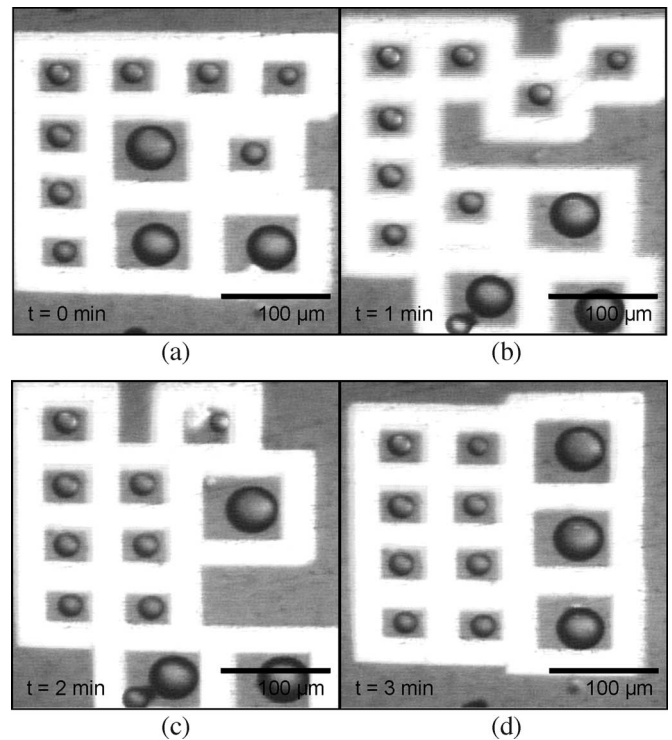


Fig. 8. Dynamic rearrangement of an array containing both 45- and 20- μm particles. An array is rearranged by moving individual cells into a desired configuration. Total rearrangement time is 3 min.

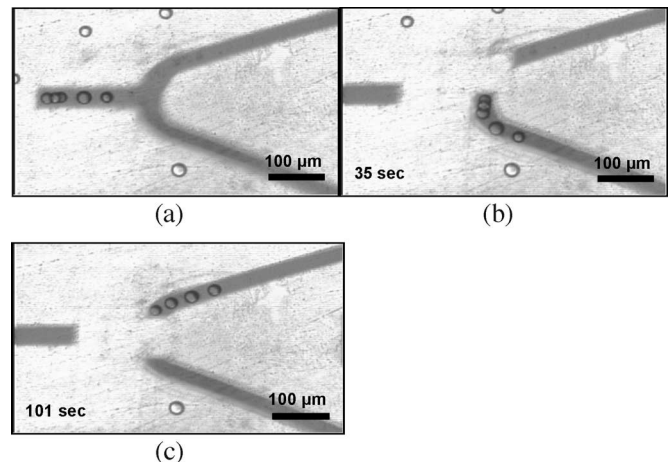


Fig. 9. (a) Polystyrene beads in a light-defined channel. The 20- μm particles can be directed down either the (b) lower branch or (c) upper branch under direct user control.

user-controlled “valves” in the channels to allow selective particle transport between channels [Fig. 9(b) and (c)].

Other patterns can be utilized for sorting particles based on size. Here, we use a “comb” configuration, which utilizes a periodic alternating illuminated/nonilluminated line (Fig. 10). This comb is swept across the manipulation area at a rate of 25 $\mu\text{m}/\text{s}$. Smaller (20- μm -diameter) beads are able to escape through the gaps in the electric field potential between the illuminated areas. However, these gaps are too small to allow the larger (45- μm -diameter) beads to escape. Thus, the smaller beads are left behind, whereas the larger beads are swept out of the manipulation area.

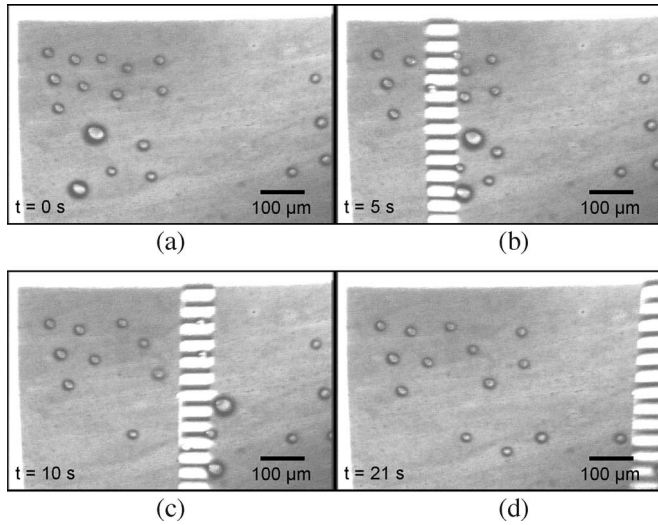


Fig. 10. Sized-based sorting of 20- and 45- μm -diameter beads. (b)–(d) “Comb” pattern is swept across the manipulation area. (b) and (c) Larger 45- μm beads are pushed to the right. (d) Smaller 20- μm beads escape through the dark gaps in the light pattern and remain in the manipulation area.

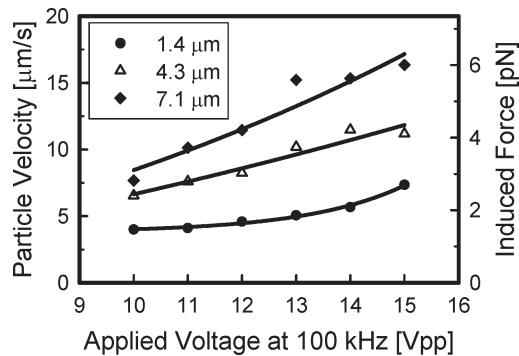


Fig. 11. Induced particle velocity (measured) and force (calculated) as a function of applied voltage at 100 kHz for several illumination pattern widths. Mean particle diameter is 20 μm .

Induced particle velocities were measured using a LED source (Luxeon Star/O, $\lambda = 625 \text{ nm}$), which provided a power density of $10.8 \text{ nW}/\mu\text{m}^2$. The maximum manipulation velocity of 20- μm -diameter beads is a function of several factors. As expected, the velocity increases as the applied voltage is increased (Fig. 11). In steady state, the OET force is balanced by the viscous drag of the fluid, which is related to the velocity of a spherical particle by Stokes' law, i.e., $F = 6\pi r\eta v$, where r is the radius of the particle, η is the viscosity of the fluid, and v is the velocity of the particle. We can therefore use Stokes' law to calculate the OET force on a particle.

Increasing the applied voltage translates into a sharper electric field gradient, increasing the DEP force [see (1)]. However, DEP forces are typically proportional to the square of the applied voltage; our results show a more linear relationship. We have also found that particle velocity is dependent on the linewidth of the manipulation pattern, which is a phenomenon that is unique to our manipulation technique (Fig. 12). The trends observed in Figs. 11 and 12 can be attributed to the tendency of polystyrene particles to levitate vertically, due to the vertical gradient of the electric field [Fig. 3(b)]. As a

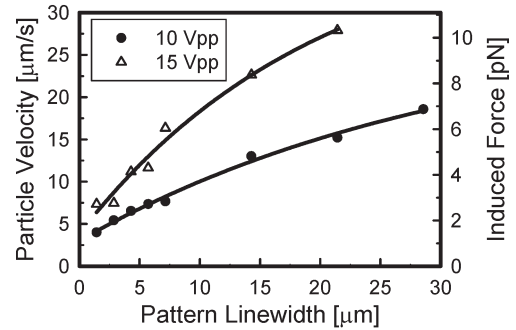


Fig. 12. Induced particle velocity (measured) and force (calculated) as a function of the illuminated linewidth of the manipulation pattern. The lower curve is for an applied bias of 10 Vpp at 100 kHz; the top curve is for a bias of 15 Vpp at 100 kHz. Mean particle diameter is 20 μm .

result, as the optical patterns are swept across the manipulation area, particles move in both the lateral and vertical directions. Furthermore, as the applied voltage is increased, both the lateral and vertical gradients increase proportionally. However, in the case of these experiments, an increase in the vertical gradient is undesirable. The increased vertical gradient will result in increased particle levitation, which reduces the lateral force induced on a particle. As a particle is levitated away from the a-Si OET surface, the lateral field gradient decreases [Fig. 3(b)], resulting in reduced lateral force. Similarly, a pattern with a narrow linewidth cannot be moved very rapidly before a particle's tendency to levitate causes it to rise over the potential “wall” created by the pattern's corresponding electric field. However, this problem is alleviated by utilizing wider linewidth patterns. It may also be possible to reduce this effect by using a smaller spacing between the top and bottom OET surfaces.

Another factor affecting single-particle manipulation velocities is the dimensions of the single-particle trap [Fig. 13(a)]. The inner trap width is the measured distance between the light patterns forming the “walls” of the trap. These data agree with simulations [Fig. 3(b)] that show that the electric field gradient extends beyond the illuminated optical pattern. This results in the levitation of particles in traps with smaller inner dimensions. This levitation, in turn, causes a reduction in the lateral induced force and makes the single-particle trap more unstable. Measurements performed with inner trap widths of less than 35 μm showed that these traps are too unstable to provide reliable particle movement in the desired direction. The corresponding simulations show [Fig. 3(b)] that for the smaller trap dimensions, the center of the trap is a local minimum. However, as the trap is moved, particles can easily migrate to the outside of the trap, which has a lower potential.

B. Mammalian Cell Manipulation

The results achieved using polystyrene beads are not exactly representative of live mammalian cells. The beads used in the OET experiments are homogeneously composed of polystyrene, whereas mammalian cells have a more complex structure consisting of a phospholipid membrane, cytoplasm, and multiple organelles. To model DEP force on cells, a single-shell representation is used [Fig. 14(a)] [28]. The permittivity and conductivity of the cell membrane and interior are used to

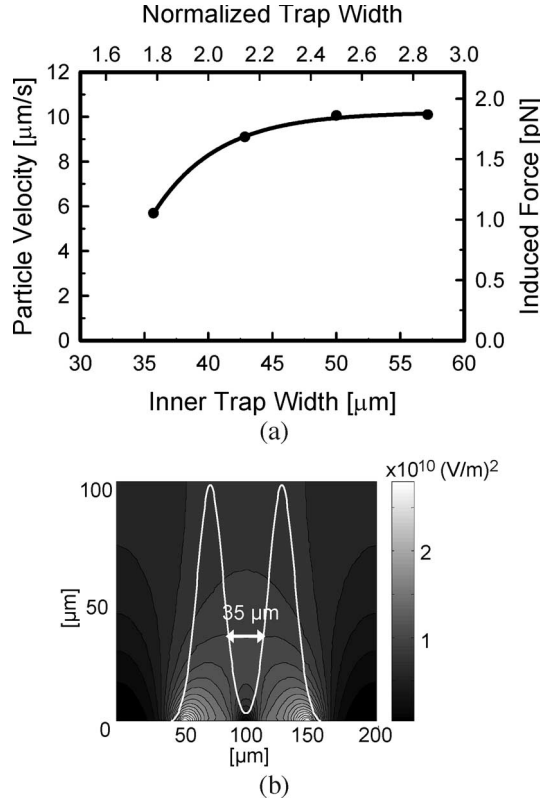


Fig. 13. (a) Induced particle velocity (measured) and force (calculated) as a function of inner trap dimensions that were measured between the light patterns forming the trap walls. Mean particle diameter is 20 μm. Applied bias is 10 V_{pp} at 100 kHz. (b) Simulated square of the electric field for a 35-μm-inner-diameter particle trap.

determine an effective complex permittivity that is used in (2). This effective permittivity is given by [28]

$$\varepsilon_p^* = C_{\text{mem}}^* \frac{3r\varepsilon_{\text{int}}^*}{3\varepsilon_{\text{int}}^* + 3C_{\text{mem}}^*r} \quad (3)$$

assuming that the thickness d of the cell membrane is much less than the radius r of the cell interior. The membrane capacitance C_{mem}^* is given by [28]

$$C_{\text{mem}}^* = \frac{\varepsilon_{\text{mem}}}{d} - \frac{j\sigma_{\text{mem}}}{d}. \quad (4)$$

A different DEP force is experienced by polystyrene beads and mammalian cells, as a result of their difference in electrical properties [Fig. 14(b)]. Typical parameters for polystyrene beads, red blood cells, and B cells were used to simulate the change in DEP response for each particle type, which was suspended in an aqueous solution with a conductivity of 10 mS/m (Table II). Empirically, this means that under the experimental conditions described in this paper, polystyrene beads will always experience a repulsive force (negative values) from the OET optical patterns. In contrast, red blood cells and B cells experience a repulsive force at lower frequencies (less than approximately 100 kHz) and an attractive force at higher frequencies (greater than approximately 100 kHz).

The concentration of bovine red blood cells was achieved using a 0.8-mW He–Ne laser ($\lambda = 633$ nm) as an optical

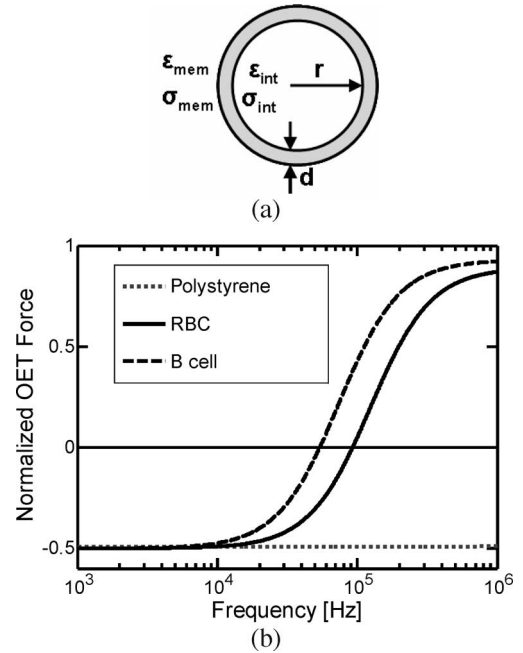


Fig. 14. (a) Single-shell model of a typical mammalian cell. (b) Normalized DEP force for three different types of microparticles in a 10-mS/m aqueous solution as a function of the frequency of the applied electric field. Positive values indicate an attractive force, whereas negative values indicate a repulsive force.

TABLE II
MICROPARTICLE PROPERTIES

	Polystyrene	Red blood cell ^a	B cell ^b
ε_r	2.55	n/a	n/a
σ	0.1 mS/m	n/a	n/a
ε_{int}	n/a	50	154
σ_{int}	n/a	0.53 S/m	0.73 S/m
C_{mem}	n/a	0.01 F/m ²	0.0126 F/m ²
Radius	n/a	2.4 μm	3.29 μm

^aRed blood cell parameters are from reference [29]

^bB cell parameters are from reference [30]

source. A spatial light modulator was not used in the setup. A 10× objective lens was used to reduce the laser beam size to ~20 μm in diameter.

A strong positive OET response was observed at an applied ac bias of 3 V_{pp} at 200 kHz, attracting the red blood cells toward the laser spot (Fig. 15). Initially, the laser is on [Fig. 15(a)], but no electric field is applied. An ac bias is then applied to the OET device, producing OET force, which attracts the blood cells to the illuminated area at velocities of up to 9 μm/s [Fig. 15(b)]. It was also observed that the cells align vertically along the electric field lines [Fig. 14(b)]. When the laser is turned off, the concentrated cells remain in the area that the laser spot was focused [Fig. 15(c)]. As the applied voltage is switched off, the concentrated red blood cells began to slowly pulsate, migrating away from the central area [Fig. 15(d)], implying that they remain alive and viable.

The patterning of live human B cells was achieved with a 100-W halogen lamp and the DMD spatial light modulator. The B cells can be manipulated into an arbitrary pattern. Here, we chose to assemble the cells into the shape of “U” and “C”

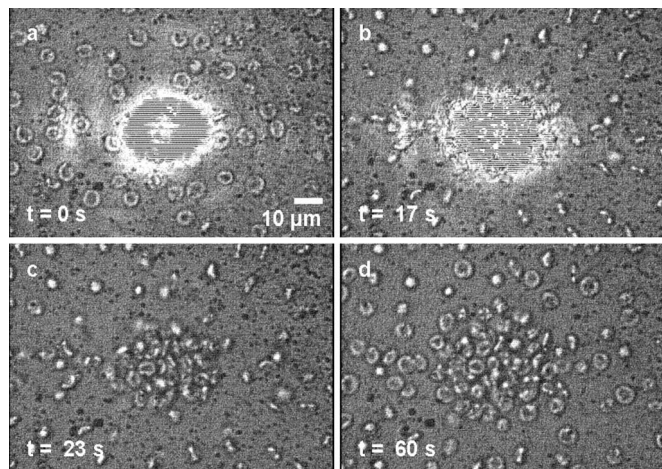


Fig. 15. Concentration of bovine red blood cells using OET. (a) Prior to applying an electric field, the blood cells are not attracted to the laser spot. (b) Applied voltage of 3 Vpp at 200 kHz is switched on. The red blood cells align vertically with the electric field and are attracted to the laser spot. (c) Laser and applied voltage are switched off. Red blood cells are clearly shown to be concentrated in the area of the laser spot. (d) Concentrated cells slowly diffuse out of the concentrated area.

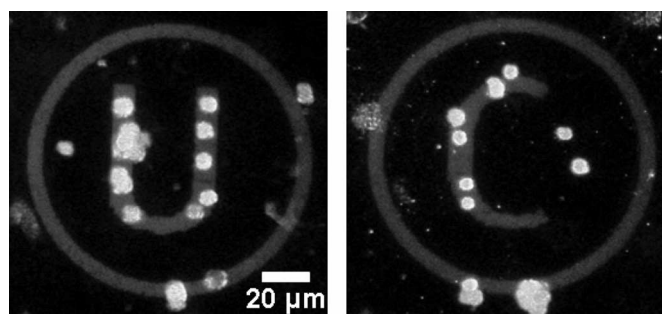


Fig. 16. Patterning of human white blood cells. Cells are attracted to the illuminated “U” and “C” characters by positive OET. The ring is part of a concentric pattern that is used to concentrate the B-lymphocytes toward the characters. Additional cells along the ring are moving in toward the characters.

characters (for University of California). At an applied bias of 14 Vpp at a frequency of 100 kHz, the white blood cells exhibit positive OET behavior. A shrinking concentric ring pattern is used to concentrate the cells toward the character image at velocities of approximately $9 \mu\text{m/s}$ (Fig. 16). Cells are attracted to each concentric ring. As the rings shrink, the cells are transported toward the center of the concentric rings, where the character image is projected. The cells then become trapped by the static character pattern. The time required to form each character is approximately 1–2 min, depending on the overall cell concentration in the sample and the local concentration of the cells in the area covered by the optical pattern.

V. DISCUSSION

OET offer a few advantages over other microparticle manipulation techniques. Conventional DEP employs static electrodes patterned with photolithographic techniques and is, thus, not reconfigurable. Furthermore, our device requires no photolithography, making fabrication easier and less expensive. Reconfigurable DEP arrays have been demonstrated using

CMOS technology [24], but these devices are complicated and expensive to fabricate. In contrast, OET devices require minimal fabrication and no photolithography. The low fabrication costs of OET make it amenable for use as a disposable device, which reduces the risk of cross-contamination of samples.

The effective manipulation area of typical optical tweezers is limited by the high-numerical-aperture objective lenses that are used to focus the laser beam. These lenses have a typical field of view of less than $100 \mu\text{m}$, limiting the parallel manipulation capabilities of larger microparticles (e.g., human lymphocytes have diameters of $\sim 10 \mu\text{m}$). Since the OET mechanism does not require a highly focused beam, low-magnification objectives allow OET to be effective over a much larger area ($1.3 \times 1.0 \text{ mm}$). We have demonstrated this by the creation of an array of 15 000 individually addressable single-particle traps over an area of 1.3 mm^2 [15]. The array consists of optically defined traps with diameters of $4.5 \mu\text{m}$, containing $4.5\text{-}\mu\text{m}$ -diameter polystyrene beads, with a trap-to-trap spacing of $9 \mu\text{m}$. However, a tradeoff exists between OET resolution and effective manipulation area; to create a more highly focused optical pattern, the effective area must be reduced. This optical pattern limitation does not apply to electrode-based DEP, where the effective manipulation area is limited only by constraints on device dimensions. However, the reconfigurable nature of OET can be used to mitigate the effects of a limited manipulation area. For example, conventional DEP sorts similarly sized particles based solely on differences in their electrical properties [21], [23], [28]. With OET, we can use visual attributes such as size, color, and texture to further differentiate between particles. Once distinguishing visual attributes have been identified using image-analysis software, the appropriate optical patterns can be generated to separate the different particles [27]. With this system, it is possible to separate particles over a smaller area than would be required otherwise.

Although holographic tweezers can generate multiple dynamic traps, direct imaging using a DMD is more versatile. Any arbitrary pattern can be generated with a high contrast ratio, without any of the computation associated with the generation of a holographic pattern. Furthermore, OET can induce repulsive forces on transparent dielectric particles such as biological cells, whereas optical tweezers is limited to attractive forces.

As OET relies on a different mechanism than optical tweezers, the optical power requirements of OET are much lower than those of optical tweezers. A typical optical tweezers trap requires at least 1 mW of optical power, whereas the creation of multiple optical traps with holographic optical tweezers requires lasers with powers of 500 mW to 1 W [5], [6]. In contrast, OET actuation has been obtained using power levels as low as $1 \mu\text{W}$, corresponding to an optical power density of $4.4 \text{ nW}/\mu\text{m}^2$ [16]. This is five orders of magnitude lower than the power density in a 1-mW optical tweezers trap that is focused at the diffraction limit. The much lower power requirements of OET actuation allow the use of inexpensive incoherent light sources. In addition, the lower power densities in OET traps lower the risk of optical damage or heating effects on live biological particles [7], [8]. The optical power density has an effect on the force induced in the OET device, as higher

optical intensities further reduce the impedance of the a-Si layer. In the experiments described here, the incoherent light sources do not generate sufficient optical intensities to fully turn on the virtual electrode that is created by the optical pattern. As a result, the OET forces are lower than in previous results [16] and similar electrode-based DEP devices. Stronger OET forces may be obtained by increasing the intensity of the optical source or by improving the photoresponse of the a-Si layer.

The photoconductivity of the a-Si layer also limits the conductivity of the liquid layer. As described earlier, OET relies on the switching of the applied voltage between the liquid and a-Si layers of the OET device. Thus, the impedance of the illuminated a-Si must be less than that of the liquid layer. While this condition is met by low-conductivity media such as those used in the experiments described here, high-conductivity media such as cell culture media is incompatible with OET operation. Our group is currently working on improving the OET device for use with high-conductivity liquids.

We envision the OET device as a tool to complement conventional DEP and optical tweezers. The optically patterned electrodes of OET allow greater flexibility than those of conventional DEP, such as the ability to isolate specific single particles from a mixed population, which could be useful in applications such as stem-cell research. In addition, the optical requirements for OET are more relaxed than those for optical tweezers, offering greater flexibility in optical sources and reducing the risk of photodamage to the particles under manipulation. The flexibility and dynamic control of OET manipulation will provide a powerful tool in biological experiments.

VI. CONCLUSION

We have demonstrated optical particle manipulation using *incoherent* light. By integrating a spatial light modulator and direct imaging with OET, many dynamic reconfigurable manipulation patterns can be employed. Using a variety of patterns, we have realized live cell and microparticle collectors, single-particle traps, and individually addressable single-particle arrays. In addition, we have achieved other manipulation functions unique to OET-based manipulation, such as light-defined particle channels and size-based particle sorting with a comb sorter. Such particle manipulation techniques have many applications to experiments with biological cells and microparticles.

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